



# Investigation on phase and microstructures of a temperature stable high-Q $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$ microwave dielectric ceramic

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## Abstract

A temperature stable high-Q  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  microwave dielectric ceramic is fabricated by conventional solid-state reaction route and the phase composition, microstructures and microwave dielectric properties are investigated in this paper. The bulk density and FESEM results indicate that this ceramic can be well-sintered at 1075 °C for 4 h. Since the difficulty in  $\text{Sr}^{2+}$  ions diffused into the  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  crystal lattice to form solid solutions owing to the large radii difference between  $\text{Sr}^{2+}$  (1.44 Å) and  $\text{Zn}^{2+}$  (0.74 Å), there are three phases including the main phase  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  and the second phase  $\text{SrTiO}_3$  and unknown phase according to the XRD and element-distribution mapping results. The formation of second phase is advantageous to improve the relative permittivity ( $\epsilon_r$ ) and temperature coefficient of resonant frequency ( $\tau_f$ ), but degrades the quality factor ( $Q \times f$ ) slightly. The  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramic sintered at 1075 °C/4 h displays a temperature stable high-Q properties:  $\epsilon_r = 26.6$ ,  $Q \times f = 62300$  GHz, and  $\tau_f = 0.27$  ppm/°C.

## 1 Introduction

In the era of information explosion, high performance microwave dielectric ceramics as the basic materials of filter, antenna and resonator components play a more and more important role in new-style telecommunication technology such as fifth generation wireless systems, internet of things, the industrial internet, satellite broadcasting, intelligent transport systems and so on [1, 2]. There are three properties simultaneously satisfied for ideal microwave dielectric ceramic materials from the device design point of view: appropriate relative permittivity ( $\epsilon_r$ , low- $\epsilon_r$  for millimeter-wave communication and substrate materials, medium- $\epsilon_r$  for satellite communications and cellphone base stations, and high- $\epsilon_r$  for miniaturization of mobile terminal equipment), high quality factor ( $Q \times f \geq 50,000$  GHz, for the good frequency selectivity of device), near zero temperature

coefficient of resonant frequency ( $\tau_f \leq \pm 10$  ppm/°C, for the stability of the frequency against temperature change) [2, 3]. Unfortunately, most of these ceramic materials with appropriate relative permittivity and high quality factor cannot be used for commercial application due to excessive positive or negative zero temperature coefficient of resonant frequency. Therefore, it is both a key and a difficult point to adjust the  $\tau_f$  to near zero and maintain high  $Q \times f$  value as much as possible synchronously.

Nowadays, there are two dominant methods applied for producing a material with near zero temperature coefficient of resonant frequency [4, 5]: (a) Composite materials by mixing component materials with negative and positive  $\tau_f$  values, such as  $\text{Mg}_4\text{Ta}_2\text{O}_9$  (−70 ppm/°C)– $\text{MgTa}_2\text{O}_6$  (+56 ppm/°C) [6],  $\text{Li}_2\text{Zn}_3\text{Ti}_4\text{O}_{12}$  (−48 ppm/°C)– $\text{TiO}_2$  (+456 ppm/°C) [5],  $\text{Mg}_6\text{Ti}_5\text{O}_{16}$  (−50 ppm/°C)– $\text{Ca}_{0.8}\text{Sr}_{0.2}\text{TiO}_3$  (+991 ppm/°C) [7]. (b) Solid solutions ceramic materials through adjustment structure, for instance  $\text{A}(\text{B}'_{1/3}\text{B}''_{2/3})\text{O}_3$  ( $\text{A} = \text{Sr}, \text{Ba}$ ,  $\text{B}' = \text{Zn}, \text{Mg}$ ,  $\text{B}'' = \text{Ta}, \text{Nb}$ ) complex perovskite system and  $(\text{Zr}, \text{Sn})\text{TiO}_4$  system [8–10]. Recently,  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  ceramic has been extensively investigated because of low sintering temperature (1075 °C for 4 h) and good microwave dielectric properties ( $\epsilon_r = 25.6$ ,  $Q \times f = 72,000$  GHz and  $\tau_f = -11.2$  ppm/°C) [11]. These advantages make it as a promising material for the applications in dielectric antennas and dielectric resonators except for excessive negative  $\tau_f$  value which impedes its application. In fact, some work has been done to modify the

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$\tau_f$  value to near-zero by adding large positive  $\tau_f$  (e.g.  $\text{TiO}_2$ ,  $\text{CaTiO}_3 + 859 \text{ ppm/}^\circ\text{C}$ ) [5, 12]. For instance, Bari et al. [4] reported that the  $\text{TiO}_2$  nanoparticles additive on  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  ceramic not only obtained optimal dielectric properties ( $\epsilon_r = 28$ ,  $Q \times f = 68,000 \text{ GHz}$ , and  $\tau_f = -2 \text{ ppm/}^\circ\text{C}$ ), but also the sintering temperature was reduced to  $1050^\circ\text{C}$ . George and Sebastian [12] found that when Ca ion substitutes for Zn ion of  $\text{Li}_2\text{ZnTi}_3\text{O}_8$ , the second phase  $\text{CaTiO}_3$  phase form in  $\text{Li}_2(\text{Zn}_{1-x}\text{Ca}_x)\text{Ti}_3\text{O}_8$  ( $0 \leq x \leq 0.2$ ) system, which can make the  $\tau_f$  value of  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  to near zero due to the large positive  $\tau_f$  of  $\text{CaTiO}_3$  phase. Typically, the  $\text{Li}_2\text{Zn}_{0.095}\text{Ca}_{0.05}\text{Ti}_3\text{O}_8$  ceramics displayed excellent comprehensive properties of  $\epsilon_r = 27$ ,  $Q \times f = 40,000 \text{ GHz}$  and  $\tau_f = -2 \text{ ppm/}^\circ\text{C}$ . Hence, it is effective method for adjusting the  $\tau_f$  of  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  ceramic to near-zero by mixing with the positive  $\tau_f$  value of ceramic materials. Besides,  $\text{SrTiO}_3$  ceramic has bigger positive  $\tau_f$  value than  $\text{CaTiO}_3$ . In present paper, the sintering behaviors, phases, microstructures and microwave dielectric properties of  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramic will be investigated in detail.

## 2 Experimental

The  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  powders were synthesized by the conventional solid-state-reaction method using stoichiometry of high-purity raw materials (99.9%, Sinopharm Chemical Reagent Co. Ltd, China), namely  $\text{Li}_2\text{CO}_3$ ,  $\text{ZnO}$ ,  $\text{SrCO}_3$  and  $\text{TiO}_2$ . The mixture mixed in a Nylon tank using ethyl alcohol and  $\text{ZrO}_2$  balls as media by planetary ball mill for 2 h were dried at  $110^\circ\text{C}$  for 4 h and then calcined at  $900^\circ\text{C}$  for 8 h. Subsequently, the calcined powders were planetary-milled with  $\text{ZrO}_2$  balls and ethyl alcohol for 2 h. After drying, the obtained powder were granulated by adding 8 wt.% polyvinyl alcohol solution and screened through a 40-mesh sieve for getting the uniformity particle size and good fluidity power. Preformed pellets of 15 mm in diameter and 8 mm in height were obtained from the powder using a cylindrical steel mold, and then were pressed at 2 MPa by hydraulic pressing, followed by sintering between  $1000^\circ\text{C}$  and  $1125^\circ\text{C}$  for 4 h in air at a heating rate of  $5^\circ\text{C/min}$ .

The phase compositions present in sintered samples were identified by X-ray diffraction analysis with a  $\text{Cu/K}\alpha$  radiation (XRD, D8 ADVANCE, Bruker, Germany). The microstructure characteristics of the sintered samples was observed by field emission scanning electron microscope (FESEM, Magellan 400, FEI Company, USA) equipped with an energy dispersive spectroscopy (EDS). The bulk density of sintered samples was measured applying the Archimedes' method. The dielectric constant and dielectric loss ( $\tan\delta$ ) of the samples with the diameter of 12 mm and the height of 6 mm were collected by the Hakki–Coleman dielectric resonator method in the TE011 mode using an Agilent E8363A PNA series network analyzer. The Q value were

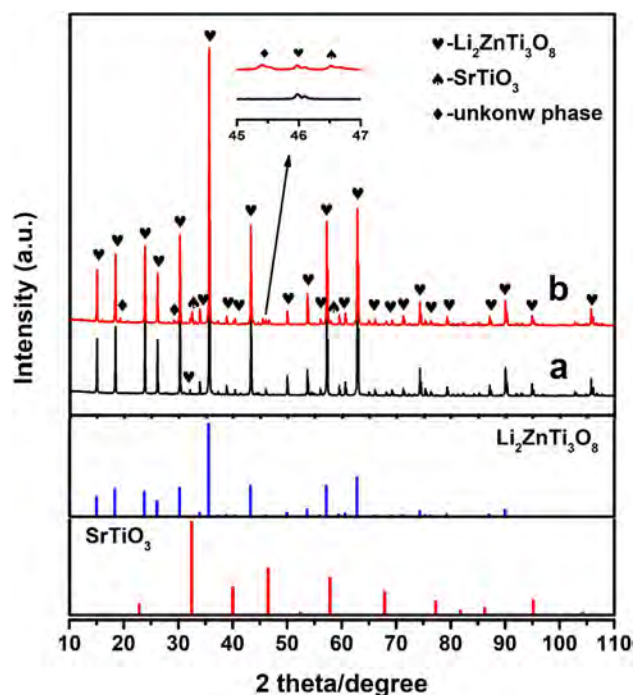
calculated from the value in the light of the  $Q = 1/\tan\delta$ . The  $\tau_f$  value was measured over the range from 25 to  $85^\circ\text{C}$  heating through the temperature test cabinet (VTL7003, Vötsch, Germany), and was calculated by following equation:

$$\tau_f = \frac{f_{85} - f_{25}}{60 \times f_{25}} \times 10^6 (\text{ppm/}^\circ\text{C})$$

where  $f_{85}$  and  $f_{25}$  represent the resonant frequencies at  $85^\circ\text{C}$  and  $25^\circ\text{C}$ , respectively.

## 3 Results and discussion

Figure 1 shows the X-ray diffraction patterns of  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  and  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramics sintered at  $1075^\circ\text{C}$  for 4 h. It can be found from Fig. 1a that the pure phase of the cubic spinel structure  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  (JCPDS no. 44-1037, P4332 (212)) ceramic is formed and there are no additional diffraction peaks to indicate secondary phase existed, such that the as-sintered sample is single-phase pure. However, the weak diffraction peaks of secondary phase corresponding to cubic structure  $\text{SrTiO}_3$  (JCPDS no. 35-0734, Pm-3m (211)) and unknown phase appeared in the XRD patterns shown in Fig. 1b of  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  as-sintered samples except for the high peaks of  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  phase. The appearance of the second phase might be ascribed to the fact that the difficulty in Sr ions diffuses into the  $\text{Li}_2\text{ZnTi}_3\text{O}_8$



**Fig. 1** XRD patterns of  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  (a) and  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  (b) ceramics sintered at  $1075^\circ\text{C}$  for 4 h

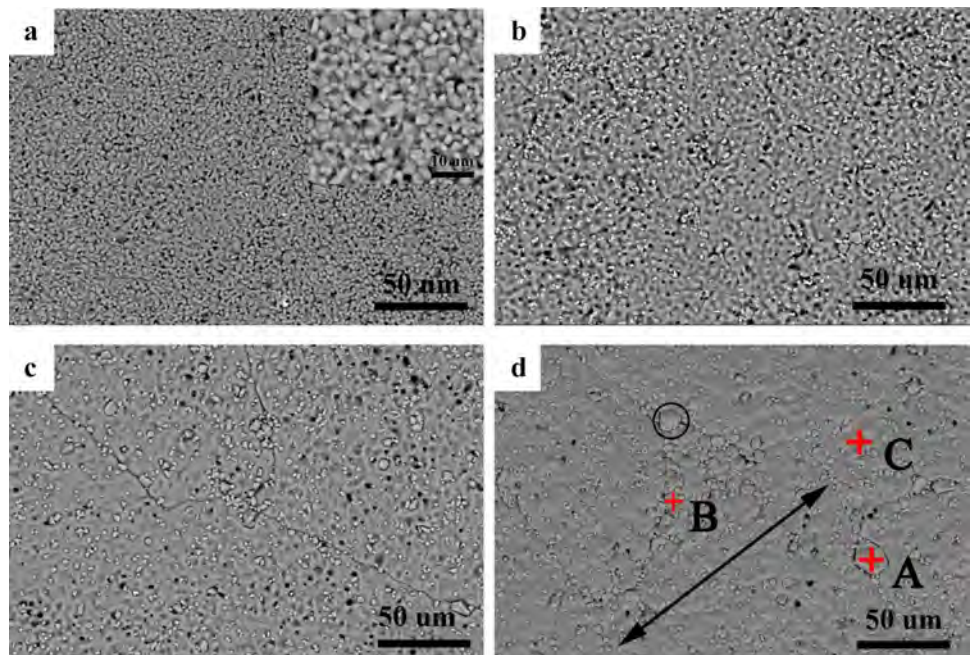
crystal lattices and forms solid solutions due to relatively large Sr ions ( $1.44\text{\AA}$ ) compared to Zn ions ( $0.74\text{\AA}$ ) [1]. This results is consistent with the Fang, George and Zhao [12–14] reports that when Ca ions substituted for Zn or Mg ions in  $\text{Li}_2\text{O}-\text{AO}-\text{TiO}_2$  ( $\text{A}=\text{Zn, Mg}$ ) system, the secondary phase  $\text{CaTiO}_3$  was obtained in this system that is advantageous to adjusting the dielectric properties, near-zero  $\tau_f$  value in particular, and reducing the Li evaporation during sintered process. Hence, the formation of  $\text{SrTiO}_3$  phase in our work will help  $\tau_f$  value of  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  shift to near zero by mixing component materials with negative and positive  $\tau_f$  values.

Figure 2 displays the SEM microstructures of natural surface of  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramics sintered at various temperatures from 1000 to 1075 °C for 4 h. As Fig. 2a shown, a porous microstructure with fine particle size (less than 10  $\mu\text{m}$ , inset) can be seen for sample sintered at 1000 °C. With the sintered temperature increasing to 1050 °C, the densification of specimen gradually increases that there are few pores around the grain boundaries and yet some pores distributed on the big grains presented in Fig. 4b–c. Beyond that, it is found that two sizes of grain, large one more than 100  $\mu\text{m}$  (see arrow) and small one (circle) still about 10  $\mu\text{m}$ , in these microstructures. To identify the chemical composition of two grains, the element-distribution mapping (EDM) and energy dispersive X-ray analysis (EDX) is carried out on natural surface of ceramic sintered at 1075 °C for 4 h shown in Figs. 3 and 4. It can be seen from Fig. 3 that large grains has a composition rich in O, Zn and Ti element and meanwhile the EDX analysis of Spot C explains that they mainly contain O, Zn and Ti elements in an approximate molar ratio of  $\text{O}:\text{Zn}:\text{Ti}=8:3:1$ , indicating that these grains

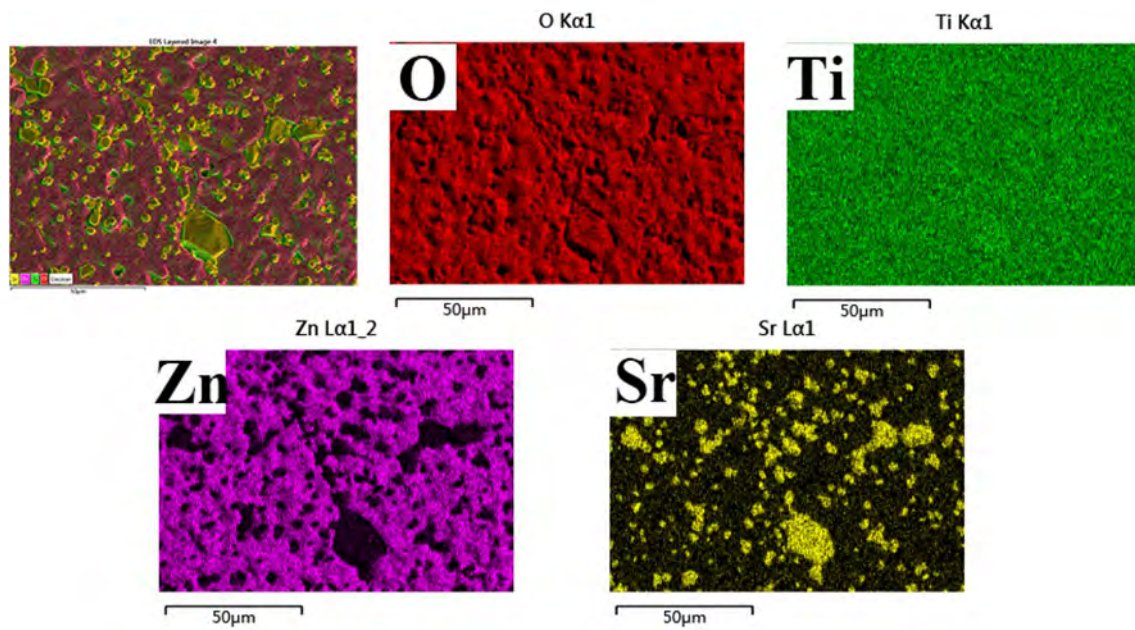
is  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  phase. The small grains are richer in O, Sr and Ti element, but the EDX data of small grains (marked A and B) reveal that these is minute quantities of Zn elements expect for primary O, Ti and Sr. It means that ZnO ion maybe react with SrO and  $\text{TiO}_2$  phase leading to form unknown phase during sintering process, and small grains include  $\text{SrTiO}_3$  phase and unknown phases. This results also illustrate that with increasing of sintering temperature the  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  grains gradually grow up and yet  $\text{SrTiO}_3$  phase grains remain the same due to higher densification temperature (1300–1400 °C) of  $\text{SrTiO}_3$  ceramic. Sintering temperature further to 1075 °C, the amount of the pore on  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  grains decreases and the sizes of  $\text{SrTiO}_3$  grains increases somewhat.

Figure 5 summaries the bulk density (a), relative permittivity (b) and  $Q \times f$  value (c) of  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramic as a function of temperature for 4 h. It is noticed from Fig. 5a that the bulk density of sintered samples increases from 3.45 to 3.98  $\text{g}/\text{cm}^3$  with increasing the sintering temperatures from 1000 to 1075 °C, and then slightly declines after 1075 °C, implying the substitution Sr for Zn has no impact on the densification process of ceramic. The variation of the relative permittivity and  $Q \times f$  value in regard to temperature has a similar tendency with bulk density as shown in Fig. 5b, c. For microwave dielectric composite ceramics, relative permittivity is dictated to sintering densification, the phase composition and its relative contents [15]. Obviously, the relative permittivity raises from 25.8 to 26.6 with the increasing sintering temperature from 1000 to 1075 °C due to the densification process. It is noteworthy that the permittivity of  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramic is higher than that of

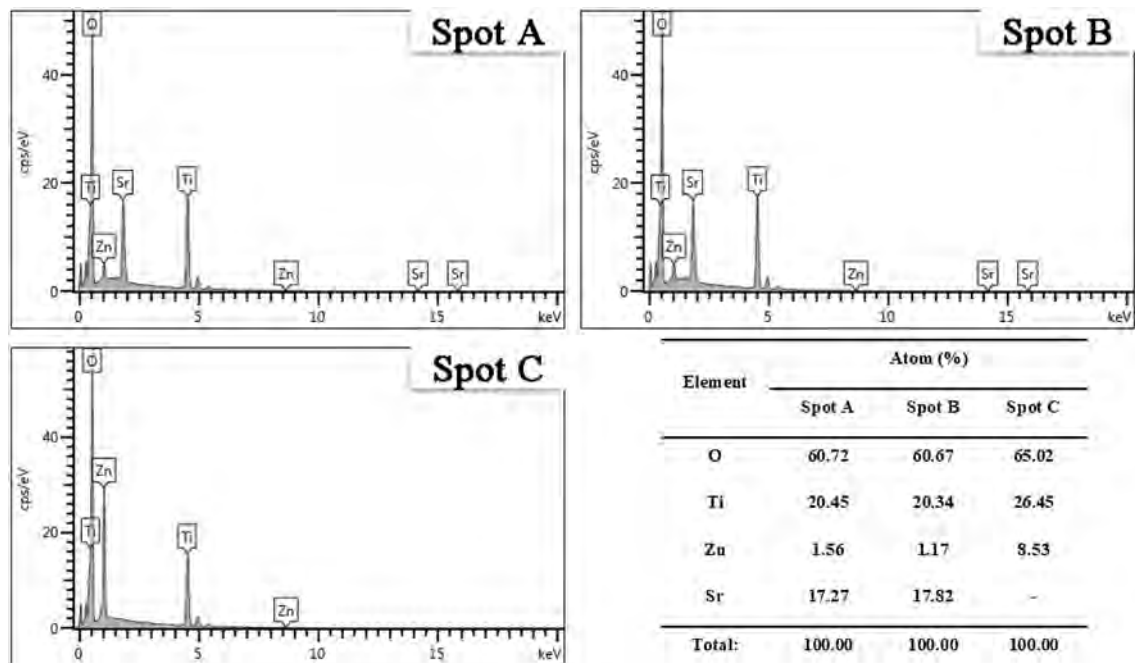
**Fig. 2** The SEM microstructures of the surface of  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramics sintered at various temperature: **a** 1000, **b** 1025, **c** 1050, **d** 1075 °C for 4 h







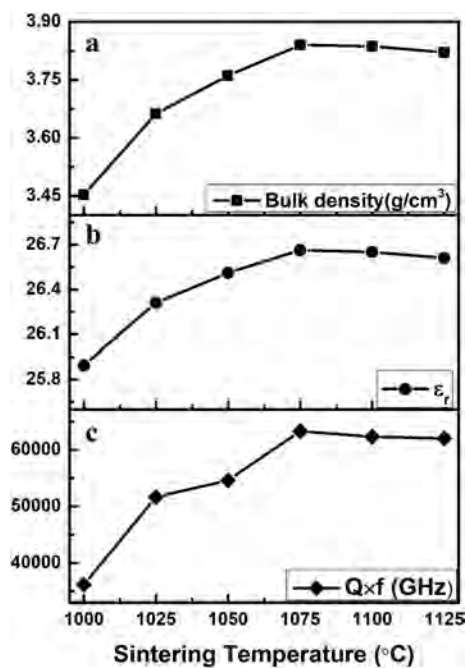
**Fig. 3** The element-distribution mapping of  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramics sintered at 1075 °C for 4 h



**Fig. 4** The energy dispersive X-ray analysis and data on the marked areas of  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramics sintered at 1075 °C for 4 h

pure  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  ceramic (25.6), and this could be the reason for the appearance formation of high- $\epsilon_r$   $\text{SrTiO}_3$  phase. The microwave dielectric loss for composite ceramics is mainly caused by the porosity, second phases, grain sizes, etc. [16]. In this case, the porosity and second phases mainly dominate the dielectric loss. The highest  $Q \times f$  value (63,000 GHz)

are obtained at 1075 °C when maximum sintering density are observed. All in all, the promising microwave dielectric properties of  $\epsilon_r = 26.6$ ,  $Q \times f = 62,300$  GHz, and  $\tau_f = 0.3$  ppm/°C can be obtained at 1075 °C for 4 h. Table 1 exhibits comparison of the microwave dielectric properties of recently reported  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  ceramic materials, which



**Fig. 5** The bulk density (a), relative permittivity (b) and  $Q \times f$  value (c) of  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramic as a function of temperature for 4 h

demonstrates that the  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramic material in our work displays excellent comprehensive microwave dielectric properties with high  $Q \times f$  value and near zero  $\tau_f$  value synchronous.

## 4 Conclusions

In the paper, the temperature stable high- $Q$   $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramic material has been synthesized and investigated. The results show that there are three phases including main phase  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  and second phase  $\text{SrTiO}_3$  and unknown phase in this ceramic sintered at 1075 °C for 4 h. With the increase of sintering temperature from 1000 to 1125 °C, the bulk density,  $\epsilon_r$  and  $Q \times f$  value of  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramic firstly increase and then decrease. The highest  $\epsilon_r$  (26.6) and  $Q \times f$  value (62,300 GHz) are obtained at 1075 °C when maximum sintering density (3.98 g/cm³) are observed, which  $\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$  ceramic has optimal comprehensive microwave dielectric properties with high  $Q \times f$  value and near zero  $\tau_f$  value (0.3 ppm/°C) synchronous.

**Table 1** The microwave dielectric properties and sintering temperature of recently reported  $\text{Li}_2\text{ZnTi}_3\text{O}_8$  ceramic materials

Composition	$\epsilon_r$	$Q \times f$ (GHz)	$\tau_f$ (ppm/°C)	$T_s$ (°C)	Second phase	Refs.
$\text{Li}_2\text{ZnTi}_3\text{O}_8$	25.6	72,000	-11.2	1075 °C/4 h	—	[11]
4 wt% nano- $\text{TiO}_2$ + $\text{Li}_2\text{ZnTi}_3\text{O}_8$	28	68,000	-2	1050 °C/4 h	$\text{TiO}_2$	[4]
Pretreating raw materials $\text{Li}_2\text{ZnTi}_3\text{O}_8$	25.8	74,200	-13	950 °C/4 h	—	[17]
Reaction sintering process $\text{Li}_2\text{ZnTi}_3\text{O}_8$	23.3	77,100	-12.4	1025 °C/4 h	—	[18]
Annealing treatment $\text{Li}_2\text{ZnTi}_3\text{O}_8$	25.6	90,000	-10.8	1075 °C/4 h	—	[19]
Controlled heating rates $\text{Li}_2\text{ZnTi}_3\text{O}_8$	26.6	83,000	-12.4	1075 °C/4 h	—	[20]
$\text{Li}_2\text{Zn}_{1.06}\text{Ti}_3\text{O}_8$	25.5	63,000	-18	1075 °C/4 h	—	[21]
$\text{Li}_2\text{Zn}(\text{Ti}_{0.93}\text{Zr}_{0.07})_3\text{O}_8$	25.4	122,000	-16	1100 °C/4 h	$\text{ZrO}_2$	[22]
$\text{Li}_2\text{ZnTi}_3\text{O}_8$ -0.2 mol $\text{SnO}_2$	20.9	89,500	-24	1080 °C/4 h	$\text{SnO}_2$	[23]
$\text{Li}_2\text{Zn}_{0.94}\text{Mg}_{0.06}\text{Ti}_3\text{O}_8$	26.1	150,000	-13.9	1140 °C/2 h	—	[24]
$\text{Li}_2\text{Zn}_{0.92}\text{Co}_{0.08}\text{Ti}_3\text{O}_8$	24.7	140,000	-13.4	1140 °C/2 h	—	—
$\text{Li}_2\text{Zn}_{0.94}\text{Co}_{0.06}\text{Ti}_3\text{O}_8$	26.2	90,400	-11.4	1075 °C/4 h	—	[25]
$\text{Li}_2\text{ZnTi}_3\text{O}_{8-x}\text{Al}_2\text{O}_3$ ( $x=0-8$ wt.%)	26.2~17.9	66,000~30,000	-11.6~-17.9	1075~1150 °C/4 h	$\text{TiO}_2$ $\text{ZnAlO}_3$	[26]
$\text{Li}_2\text{Zn}_{0.95}\text{Ca}_{0.05}\text{Ti}_3\text{O}_8$	27	52,000	-3	1075 °C/4 h	$\text{CaTiO}_3$	[12]
$\text{Li}_2\text{ZnTi}_{3.04}\text{O}_{8.12}$	25.8	63,400	-8.1	1100 °C/4 h	$\text{TiO}_2$	[27]
$\text{Li}_2\text{ZnTi}_{3.06}\text{O}_{8.18}$	25.9	47,500	-3.2	1100 °C/4 h	$\text{TiO}_2$	—
$\text{Li}_2\text{Zn}_{0.95}\text{Sr}_{0.05}\text{Ti}_3\text{O}_8$	26.6	62,300	0.3	1075 °C/4 h	$\text{SrTiO}_3$	This paper

$T_s$  sintering temperature, *Refs* references

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